

# Richa EnviRonmEntal SERvicES PRivatE l imitEd

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## Design Calculation sheet along with assumptions

### SBR ( Sequencing Batch Reactor ) – 450 KLd STP ( Sewage Treatment Plants )

#### Important

In case of SBR only.

1. The hydraulic retention time is not a basis of design , although it appears in table of design parameters , It is likewise not a design criteria , **Because SBR is a batch process** , HRT ( hydraulic retention time ) has less meaning in comparison with continuous flow reactors
2. As HRT is not a design basis for SBR , that is why all other companies who say take x or y retention time , they will end up damaging the system .

#### Inlet & outlet parameters

S.no	Parameters	Inlet	Outlet	Remarks
1	BOD 5	300 mg/l	25 mg/l	In calculation we will take outlet BOD = 0
2	TSS	200 mg/l	30 mg/l	
3	NH3- N	25 mg/l	1 mg/l	
4	Ammonical nitrogen	150 mg/l	50 mg/l	
5	Total Phosphorus	10 mg/l	2 mg/l	
6	TKN	40 mg/l	5 mg/l	
7	COD	600 mg/l	150 mg/l	

#### Design Assumptions

S.no	Parameters	At Outlet	Remarks
1	F/M Ratio (kgBOD applied/kgMLSS-d)	0.13	
2	MLSS	3500 mg/l	
3	Minimum Clarifier Depth	2.75 m	
4	Net Sludge yield (kg MLSS/kg BOD5 )	0.76	
5	Wastewater Temp	25 Degree C	
6	Min Solids Retention time	8 days	Theta C ( mean cell residence

			time )
7	<b>Reactor volume decanted each Day</b>	60 %	
8	<b>Net Elevation Above Sea Level</b>	304 m	
9	<b>DO mixed liquor concentration</b>	2.5 mg/l	
10	<b>Oxygen coefficients</b> kg O2/kg BOD 5 kg O2/kg NH3- N	1.28 4.60	
11	<b>Oxygen Transfer rate of Diffusers</b>	1.25 kgO /kW-hr	
12	<b>Number of cycles per day</b> Includes two square basins for operational flexibility	4	

### A. Reactor Volume

$$\text{BOD 5 Removed (kg/d)} = [ (\text{BOD inlet} - \text{BOD Outlet}) \text{ mg/l} ] \times \text{Flow (L/day)} \times 10^{-6} \text{ (kg/mg)}$$

$$\text{BOD 5 Removed (kg/d)} = 135 \text{ kg / day}$$

$$\text{Required Aerobic Mass (kg)} = \frac{\text{BOD 5 Removed (kg/d)}}{\text{F/M Ratio (kgBOD applied/kgMLSS-d)}}$$

$$\text{Required Aerobic Mass (kg)} = 1038.46 \text{ kg MLSS}$$

$$\text{Reactor volume (low water level) (m}^3\text{)} = \frac{\text{MLSS mass (Kg)} \times 10^6 \text{ (mg/kg)}}{\text{MLSS Conc (mg/l)} \times 10^3 \text{ (L/m}^3\text{)}}$$

$$\text{Reactor volume (low water level) (m}^3\text{)} = 297 \text{ m}^3$$

Since the Decant volume represents 60 % of the total volume

$$\text{Total Reactor Volume m}^3 = 297 / (1-0.6)$$

$$= 743 \text{ m}^3 \text{ Reactor volume}$$

### B. Decant Volume

$$\begin{aligned} \text{Total Decant volume} &= \text{Total Reactor Volume m}^3 - \text{Reactor volume (low water level) (m}^3) \\ &= 743 - 297 = \mathbf{446 \text{ m}^3 \text{ Decant volume}} \end{aligned}$$

### **C. Detention Time**

$$\begin{aligned} \text{Max Detention time (hour)} &= \text{Total Reactor volume} / \text{Flow} \\ &= \mathbf{40 \text{ hours}} \end{aligned}$$

$$\begin{aligned} \text{Min Detention time (hour)} &= \text{Decant Volume} / \text{Flow} \\ &= \mathbf{23.786 \text{ hours}} \end{aligned}$$

### **D. SBR Dimensions**

$$\text{Basin Area (m}^2) = \text{Basin Volume (low water level) m}^3 / \text{Min Depth}$$

$$\text{Basin Area (m}^2) = 108 \text{ m}^2$$

$$\text{Basin Length (m)} = 10.3 \text{ m} = 11 \text{ m}$$

$$\text{Basin Depth} = \text{Total Reactor Volume} / \text{Basin Area}$$

$$743 / (11 \times 11) = 6.14 \text{ m}$$

### **E. Aeration Required**

$$\text{Nitrogenous O}_2 \text{ Demand (kg O}_2 / \text{d)} = \text{NH}_3 - \text{N oxidized (kg/d)} \times \text{kg O}_2 / \text{kg BOD}_5$$

$$\text{NH}_3 - \text{N oxidized (kg/d)} = \text{TKN removed (kg/d)} - \text{Synthesis N (kg/d)}$$

$$\begin{aligned} \text{TKN Removed} &= (40 - 5) \times 450 \times 10^{-3} \\ &= \mathbf{15.75 \text{ kg/d}} \end{aligned}$$

Synthesis N = 5% waste activated sludge of total daily sludge production

$$\text{Sludge Production (kg/d)} = \text{Net Sludge Yield (kgMLSS/kgBOD}_5) \times \text{BOD}_5 \text{ Removed (kg/d)}$$

$$\text{Sludge Production} = 0.76 \text{ (kgMLSS/kgBOD}_5) \times 135 \text{ (kg/d)} = 102.6 \text{ kg/day}$$

$$\text{Synthesis N (kg/d)} = 0.05 \times 102.6 \text{ kg/d} = \mathbf{5.13 \text{ kg/day}}$$

$$\text{NH}_3 - \text{N oxidized (kg/d)} = 15.75 \text{ kg/d} - 5.13 \text{ kg/d} = 10.62 \text{ kg / day}$$

$$\begin{aligned} \text{Nitrogenous O}_2 \text{ Demand} &= 10.62 \text{ (kgNH}_3 - \text{N oxidized/d)} \times 4.6 \text{ (kgO}_2\text{/kgNH}_3 - \text{N oxidized)} \\ &= 48.852 \text{ kgO}_2\text{/d} \end{aligned}$$

$$\text{Carbonaceous O}_2 \text{ Demand (kg O}_2\text{/d)} = \text{BOD}_5 \text{ Mass (kg/d)} \times \text{kg O}_2\text{/kg BOD}_5$$

$$\begin{aligned} \text{Carbonaceous O}_2 \text{ Demand} &= 5.13 \text{ (kg BOD}_5\text{/d)} \times 1.28 \text{ kg O}_2\text{/kg BOD}_5 \\ &= 6.5664 \text{ kg O}_2\text{/d} \end{aligned}$$

$$\text{AOR (kg/d)} = \text{Carbonaceous O}_2 \text{ Demand (kg/d)} + \text{Nitrogenous O}_2 \text{ Demand (kg/d)}$$

$$\text{AOR} = 6.5664 \text{ kgO}_2 \text{ /d} + 48.852 \text{ kgO}_2 \text{ /d} = 55.4184 \text{ kgO}_2 \text{ /d}$$

Where AOR = Actual oxygen requirement

Note : at Standard Temp & Pressure , 1 m<sup>3</sup> air = 1.29 kg weight

Oxygen in air = 21 %

#### F. Blower Usage

<i>14 hours per day</i>	<i>Based on 4 cycles per day ( 6 hour / cycle )</i>
<i>1 hour</i>	<i>Fill time</i>
<i>3.5 hour</i>	<i>React time</i>
<i>0.75 hour</i>	<i>Settle time</i>
<i>0.5 hour</i>	<i>Decant Time</i>
<i>0.25 hour</i>	<i>Idle time</i>

<i>Richa Environmental Services Private Limited</i>			
<i>Actively involved in manufacturing , installation , design</i>			
<i>Sewage Treatment Plants STP</i>	<i>Effluent Treatment Plants (ETP)</i>	<i>MBBR</i>	<i>Sequencing Batch Reactor</i>
<i>MBR ( Membrane Bio reactor )</i>	<i>Lamella Clarifier</i>		

*For feedback or any design related queries feel free to contact us .*

*Regards*

*Richa Environmental Services Private Limited*

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